

PH 625

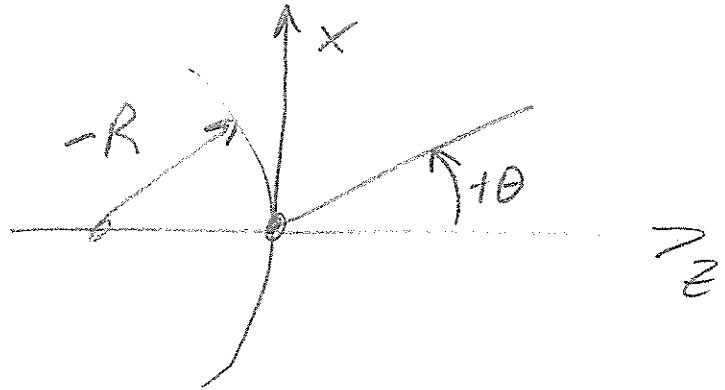
1/27/10 ①

MATRIX OPTICS

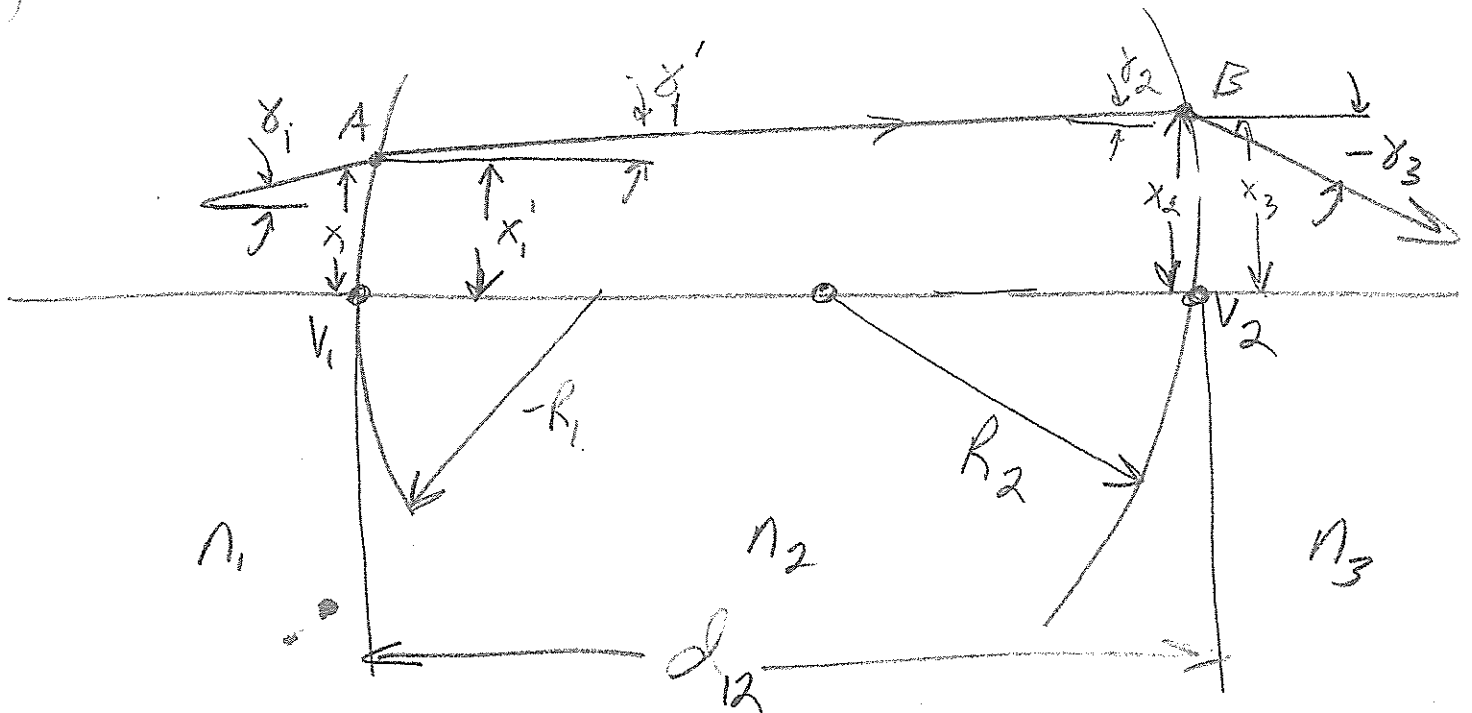
→ TODAY "ABCD" MATRIX

→ FRIDAY "EFGH" MATRIX

Sign CONVENTION:



Consider the case: Ray propagation from A to B, through an optical system



No Need to draw this!

would like to determine:

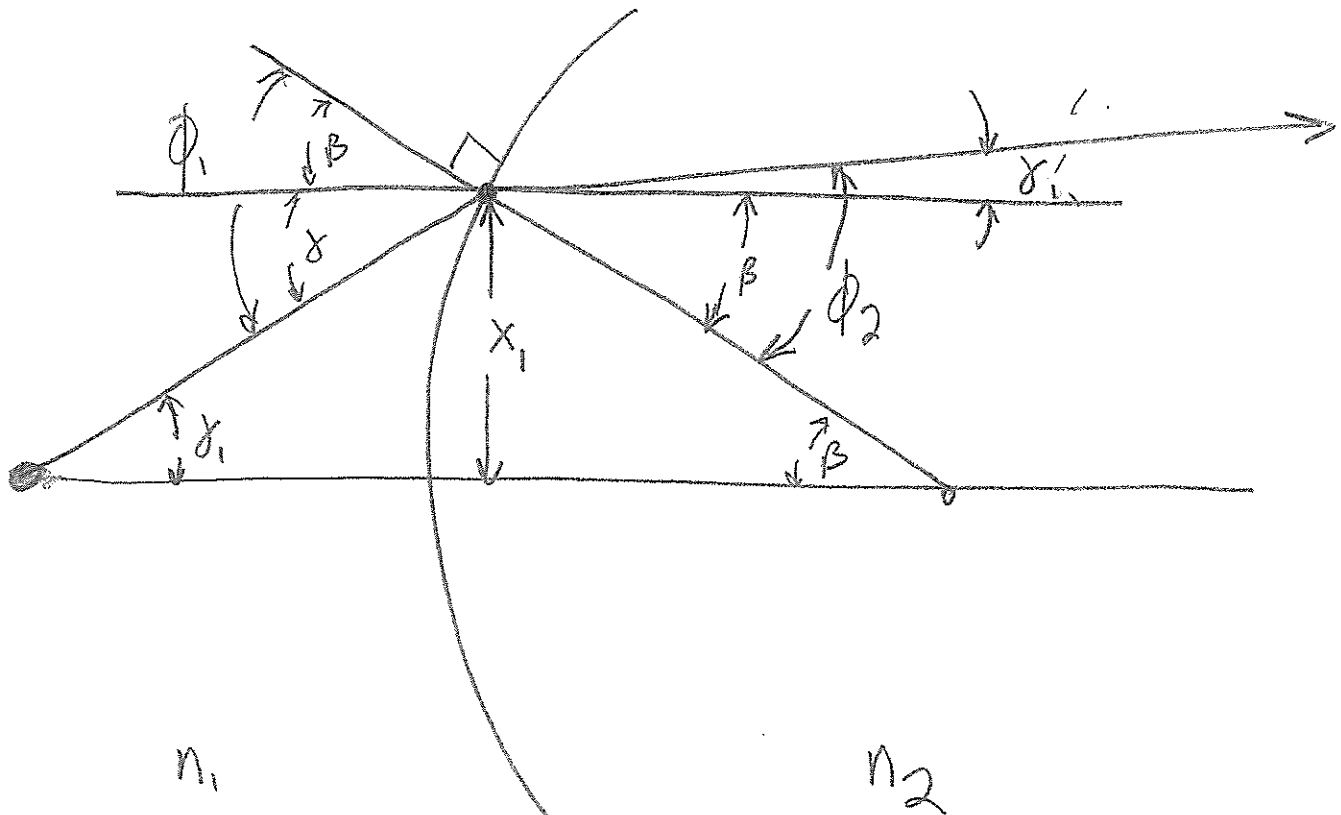
(2)

$$\begin{pmatrix} x_3 \\ y_3 \end{pmatrix} = \begin{pmatrix} g_{11} & g_{12} \\ g_{21} & g_{22} \end{pmatrix} \begin{pmatrix} x_1 \\ y_1 \end{pmatrix}$$

WHERE x_1 = Ray Height at SURFACE #1

y_1 = Ray angle in medium n_1

START WITH REFRACTION:



SNEEL:

$$n_1 \sin \phi_1 = n_2 \sin \phi_2$$

$$n_1 \phi_1 = n_2 \phi_2$$

$$\sin \phi_1 = \phi_1 - \frac{\phi_1^3}{3!} + \frac{\phi_1^5}{5!}$$

PARAXIAL APPROX = 1ST ORDER

$$\sin \phi_1 = \phi_1$$

3RD ORDER = 5TH ORDER
= ABERRATION THEORY

(3)

$$n_1 \phi_1 = n_2 \phi_2 \Rightarrow n_1 (\delta + \beta) = n_2 (\delta_1' + \beta)$$

$$n_2 \delta_1' = n_1 \delta - (n_2 - n_1) \beta$$

But $\beta = \frac{x_1}{R_1}$

$$n_2 \delta_1' = n_1 \delta - \frac{(n_2 - n_1) x_1}{R_1}$$

$$\delta_1' = \frac{n_1}{n_2} \delta - \frac{(n_2 - n_1)}{n_2} \frac{x_1}{R_1}$$

$$x_1' = x_1 + O \delta$$

$$\delta_1' = -\frac{\phi_1}{n_2} x_1 + \frac{n_1}{n_2} \delta$$

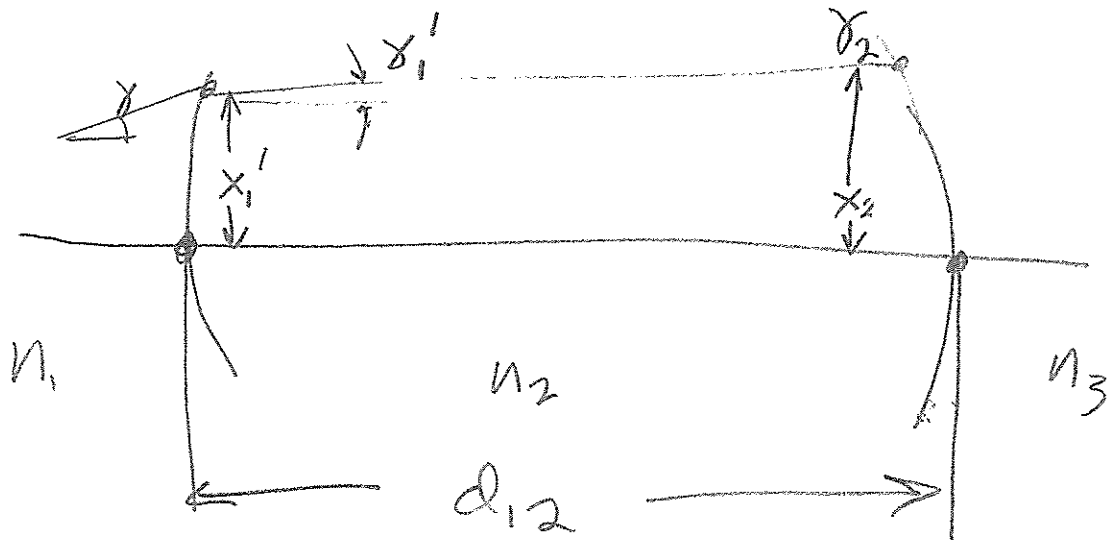
DEFINE $\phi_1 = \frac{n_2 - 1}{R_1}$

= Power

= $\frac{1}{f}$ For thin lens

$$\begin{pmatrix} x_1' \\ \delta_1' \end{pmatrix} = R_1 \begin{pmatrix} x_1 \\ \delta_1 \end{pmatrix} \quad \text{where} \quad R_1 = \begin{pmatrix} 1 & 0 \\ -\frac{\phi_1}{n_2} & \frac{n_1}{n_2} \end{pmatrix}$$

$$||R|| = \frac{n_1}{n_2}$$



$$x_2 = x_1' + \tan \delta_2 \cdot d_{12}$$

$$x_2 = x_1' + d_{12} \delta_1'$$

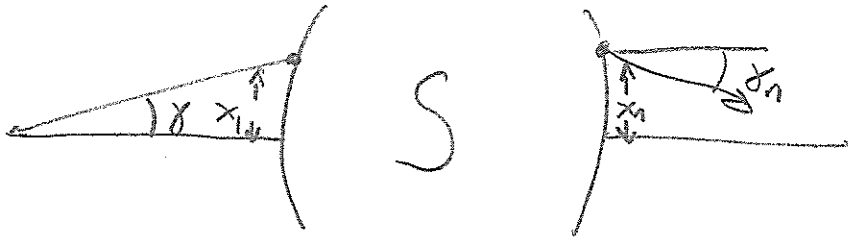
$$\delta_2 = 0 x_1 + \delta_1'$$

where

$$\begin{pmatrix} x_2 \\ \delta_2 \end{pmatrix} = T_{12} \begin{pmatrix} x_1' \\ \delta_1' \end{pmatrix} \quad T_{12} = \begin{pmatrix} 1 & d_{12} \\ 0 & 1 \end{pmatrix}$$

$$\|T_{12}\| = 1$$

(5)



$$S = R_2 T_{12} R_1$$

$$= \begin{pmatrix} 1 & 0 \\ -\frac{\phi_2}{n_3} & \frac{n_2}{n_3} \end{pmatrix} \begin{pmatrix} 1 & d_{12} \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ -\frac{\phi_1}{n_2} & \frac{n_1}{n_2} \end{pmatrix} = \begin{pmatrix} A & B \\ C & D \end{pmatrix}$$

$$A = 1 - \frac{d}{n_2} \phi_1 \quad B = \frac{d n_1}{n_2}$$

$$C = \frac{1}{n_3} \left(\phi_2 + \phi_1 - \frac{d}{n_2} \phi_1 \phi_2 \right) = \text{system power}$$

$$D = \frac{n_1}{n_3} \left(1 - \frac{d}{n_2} \phi_2 \right) = \frac{1}{S_{\text{TOTAL}}}$$

$$\|S\| = \|R_2\| \cdot \|T_{12}\| \cdot \|R_1\| = AD - BC = \frac{n_1}{n_3}$$

Thick lens in AIR
 $n_2 = n$

$$n_1 = n_3 = 1$$

$$S = \begin{pmatrix} \left(1 - \frac{\phi_1}{n} d\right) & d \\ -\left(\phi_1 + \phi_2 + \frac{\phi_1 \phi_2}{n}\right) & \left(1 - \frac{\phi_2}{n} d\right) \end{pmatrix}$$

$$\phi \equiv \frac{(n_2 - n_1)}{R_1}$$

Thin lens: special case of thick lens

$$d \ll R_1, R_2$$

$$\phi d \ll 1$$

$$S = \begin{pmatrix} 1 & 0 \\ -\phi_{\text{TOTAL}} & 1 \end{pmatrix}$$

$$\phi_{\text{TOTAL}} = \phi_1 + \phi_2 - \frac{\phi_1 \phi_2 d}{n} \approx \phi_1 + \phi_2$$

$$= \frac{n-1}{R_1} + \frac{1-n}{R_2} = n-1 \left(\frac{1}{R_1} - \frac{1}{R_2} \right)$$

$$\boxed{\phi_{\text{TOT}} \approx \frac{1}{f}}$$

SPHERICAL MIRROR (in Air)

⑥

- TREATED as a thin lens (mostly)

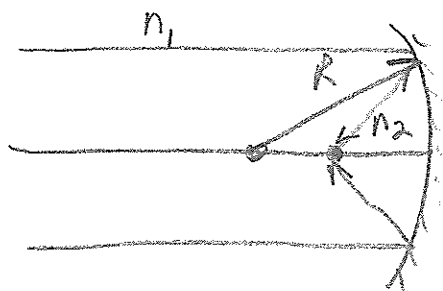
- AFTER REFLECTION

$$n_1 \rightarrow -n_2$$

$$n_2 = -n_1$$

$$\phi \equiv \frac{n_2 - n_1}{R_1}$$

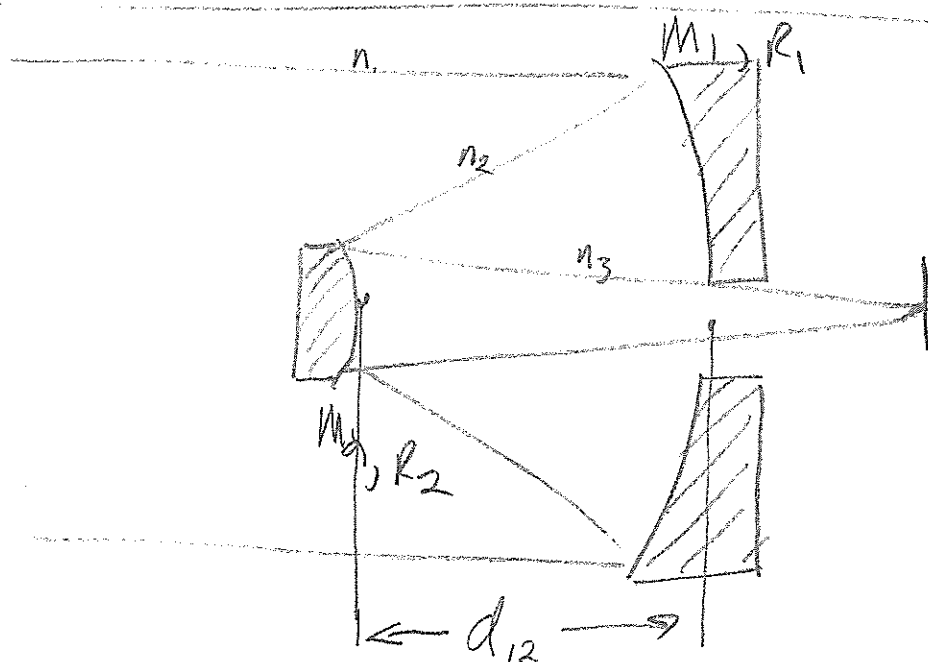
$$\phi_m = \frac{(-1) - 1}{R} = -\frac{2}{R}$$



$$R = \begin{pmatrix} 1 & 0 \\ -\phi & \frac{n_1}{n_2} \end{pmatrix}$$

$$R_m = \begin{pmatrix} 1 & 0 \\ -\frac{2}{R} & -1 \end{pmatrix}$$

$$f = \frac{1}{\phi} = \frac{R}{2}$$



KECK

$$R_1 = -34.972 \text{ m}$$

$$R_2 = -4.737 \text{ m}$$

$$d_{12} = 15.4 \text{ m}$$

Example #1

Sign convention

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Calculate the EFFECTIVE Focal length of
the KECK TELESCOPE

$$S_{\text{keck}} = R_2 T_{12} R_1$$

$$= \begin{pmatrix} 1 & 0 \\ \frac{-2}{-4.737} & -1 \end{pmatrix} \begin{pmatrix} 1 & +15.4 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ \frac{-2}{-34.972} & -1 \end{pmatrix}$$

$$= \begin{pmatrix} 1 & +15.4 \\ -0.4222 & -7.502 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ \frac{-2}{34.972} & -1 \end{pmatrix}$$

$$= \begin{pmatrix} 0.119 & -15.4 \\ 6.821 \text{E-}3 & 7.502 \end{pmatrix}$$

$$EFL = -146.604 \text{ m}$$

$$D = 10\text{-meters}$$

$$F/\# = \frac{EFL}{D}$$

$$F/\# = 14.6604$$

1/22/10 B

Example #1, the Keck Telescope

$$R2 := \begin{pmatrix} 1 & 0 \\ \frac{-2}{-4.737} & -1 \end{pmatrix} \quad R1 := \begin{pmatrix} 1 & 0 \\ \frac{-2}{-34.972} & -1 \end{pmatrix} \quad T12 := \begin{pmatrix} 1 & -15.395 \\ 0 & 1 \end{pmatrix}$$

$$SYS := R2 \cdot T12 \cdot R1$$

$$SYS = \begin{pmatrix} 0.12 & 15.395 \\ -6.7 \times 10^{-3} & 7.5 \end{pmatrix}$$

$$f := \frac{-1}{SYS_{1,0}}$$

$$f = 149.245$$

$$R3 := \begin{pmatrix} 1 & 0 \\ \frac{-1}{2.286} & 1 \end{pmatrix} \quad R4 := \begin{pmatrix} 1 & 0 \\ \frac{-1}{0.307} & 1 \end{pmatrix}$$

$$T23 := \begin{bmatrix} 1 & (17.8469 + 2.286) \\ 0 & 1 \end{bmatrix} \quad T34 := \begin{pmatrix} 1 & 2.54 \\ 0 & 1 \end{pmatrix}$$

$$SYS2 := R4 \cdot T34 \cdot R3 \cdot T23 \cdot R2 \cdot T12 \cdot R1$$

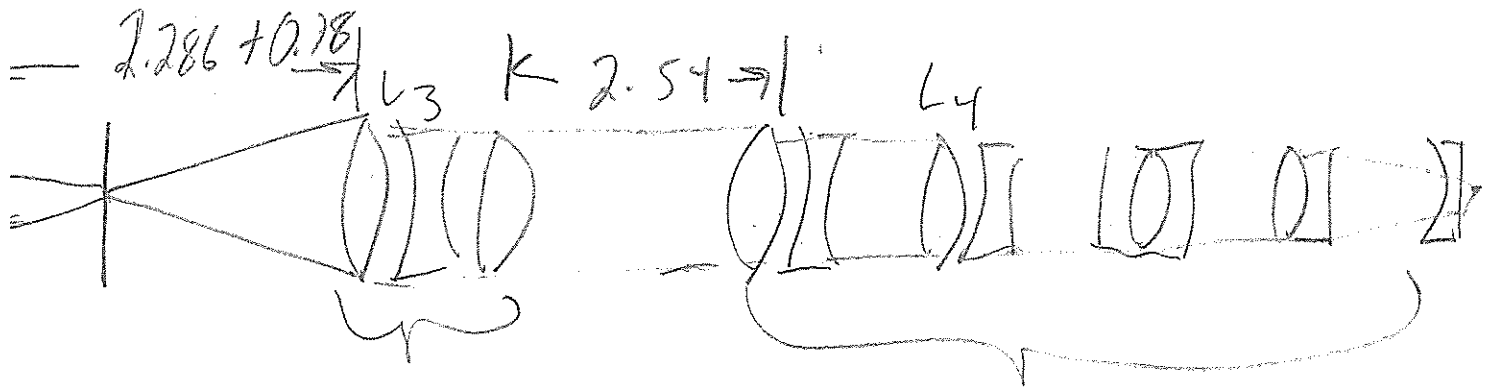
$$SYS2 = \begin{pmatrix} -0.015 & 0.562 \\ 0.05 & -67.117 \end{pmatrix}$$

$$efl := \frac{-1}{SYS2_{1,0}}$$

$$efl = -20.043$$

Ex #1 B

Keck with Echelle 11/23/10 (8)
Spectrograph; Image



$$e f l_{coll} = 2.286 \text{ m} \quad e f l_{can} = 0.307 \text{ m}$$

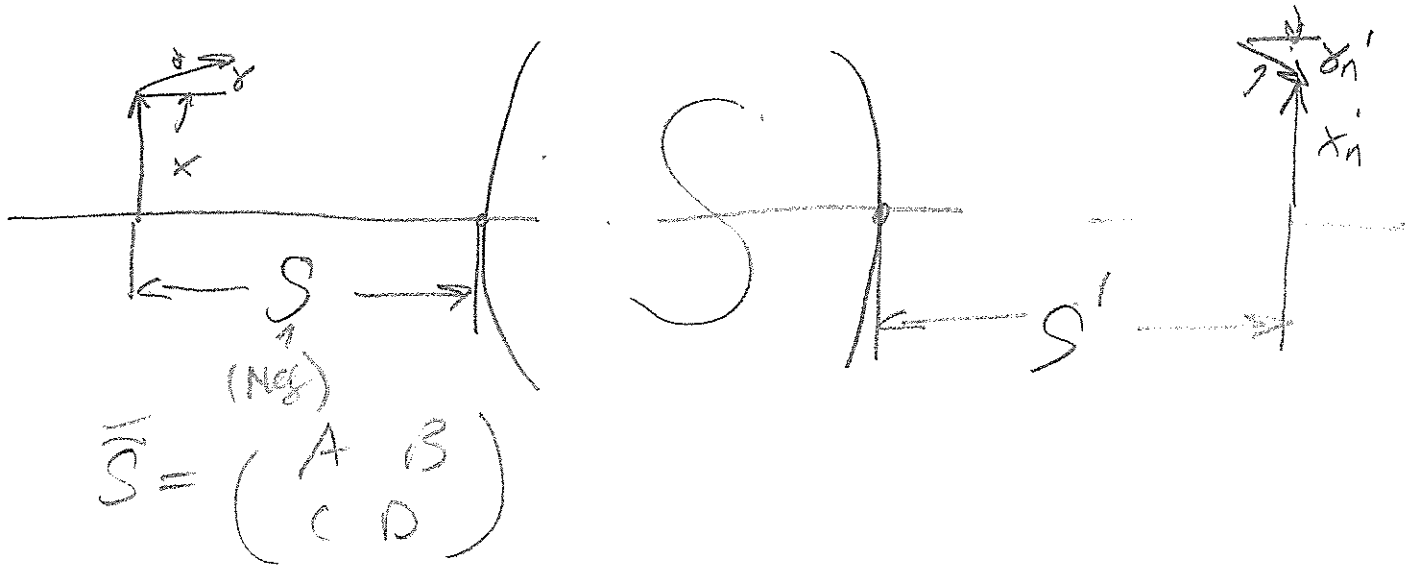
$$S_{YS} = \begin{pmatrix} -0.015 & 0.562 \\ -0.049 & -67.117 \end{pmatrix}$$

$$e f l = 20.043 \text{ m}$$

$$F/\# = 2.0043$$

Now consider OBJECT/IMAGE situation

1/29/10 ①



$$\bar{S} = \begin{pmatrix} A & B \\ C & D \end{pmatrix}$$

$$\begin{pmatrix} x' \\ y' \end{pmatrix} = \begin{pmatrix} 1 & S' \\ 0 & 1 \end{pmatrix} \begin{pmatrix} A & B \\ C & D \end{pmatrix} \begin{pmatrix} 1 & -S \\ 0 & 1 \end{pmatrix} \begin{pmatrix} x \\ y \end{pmatrix}$$

$$= \begin{pmatrix} A + S'C & B + S'D \\ C & D \end{pmatrix} \begin{pmatrix} 1 & -S \\ 0 & 1 \end{pmatrix}$$

$$= \begin{pmatrix} A + S'C & -A'S - S'S'C(B + S'D) \\ C & D - CS \end{pmatrix}$$

$$\begin{pmatrix} x' \\ y' \end{pmatrix} = \begin{pmatrix} H & G \\ F & E \end{pmatrix} \begin{pmatrix} x \\ y \end{pmatrix} = \bar{O} \begin{pmatrix} x \\ y \end{pmatrix}$$

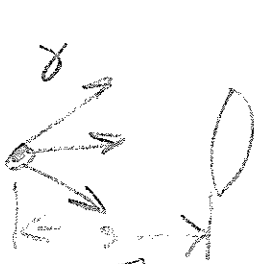
SPECIAL CASES:

(2)

$$x'_h = Hx + G\delta$$

$$\delta'_h = Fx + E\delta$$

1) $E = 0 \Rightarrow \delta' \text{ independent of } \delta \quad \delta' \sim x$



Front Focal Point

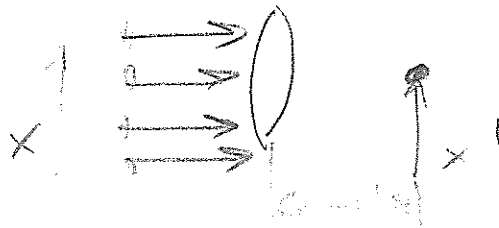
$$S = \frac{+D}{C}$$

↑
front focal point

Ray of any angle and focus height will converge at a constant angle and any height

2) $H = 0$

$$x' \text{ independent of } x \quad x' \sim \delta$$



Back Focal Point

$$S' = \frac{-A}{C}$$

↑
rear focal point

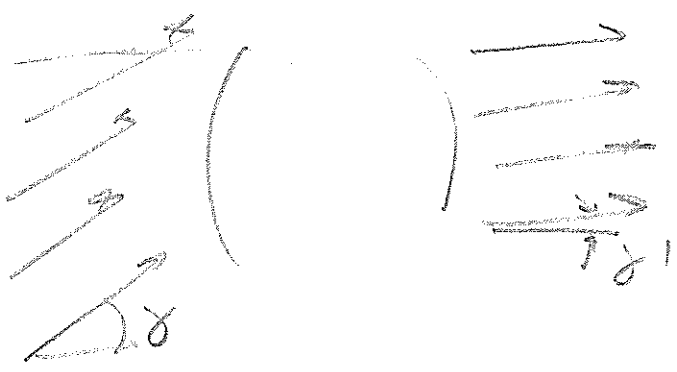
Rays of constant angle and any height will arrive at a fixed height (and any angle)

(3)

3) $E=0$

Output angle indep. of Height

DEF of Telescope



$\frac{\delta'}{\delta} = \text{Angular Mag.}$

$\frac{\delta'}{\delta} = E$

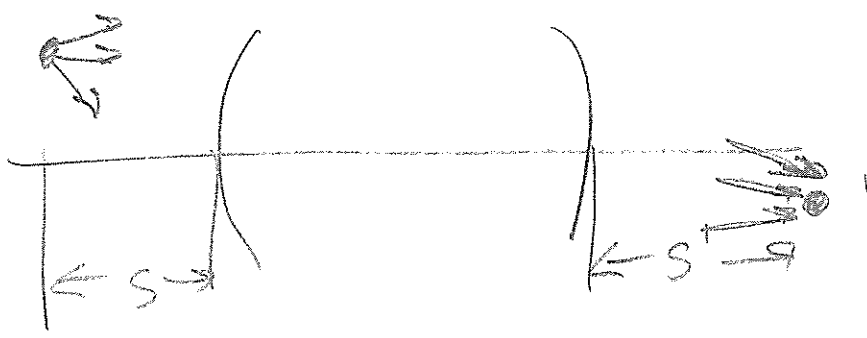
Rays of constant angle at any height will come out at

4) $G=0$

$X'_n = E \times$ Diff constant angle Any height

Image Formation

Magn. = $\frac{X'_n}{X} = H$

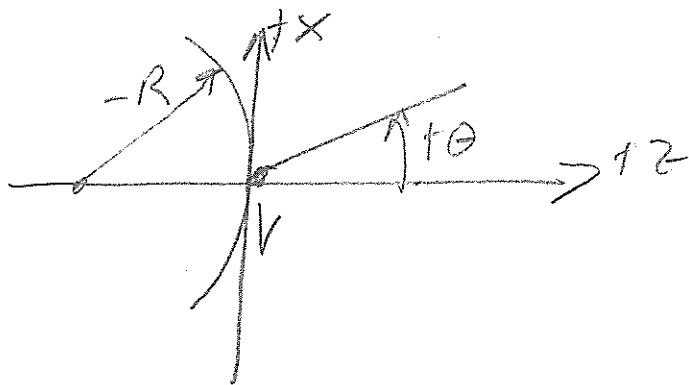


$S' = \frac{AS - B}{D - CS}$

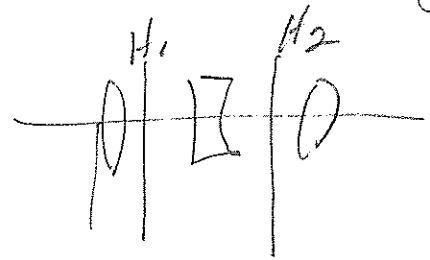
$S = \frac{B + DS'}{A + CS'}$

Image condition : Rays emitted from Fixed height arrive at fixed height independent of Angle.

Sign convention



1/29/10 (4)



IMMEDIATE FORMULAS

$$G = 0$$

$$EH = 1$$

$$\gamma = \begin{pmatrix} H & G \\ F & E \end{pmatrix}$$

$$EH - FG = 1$$

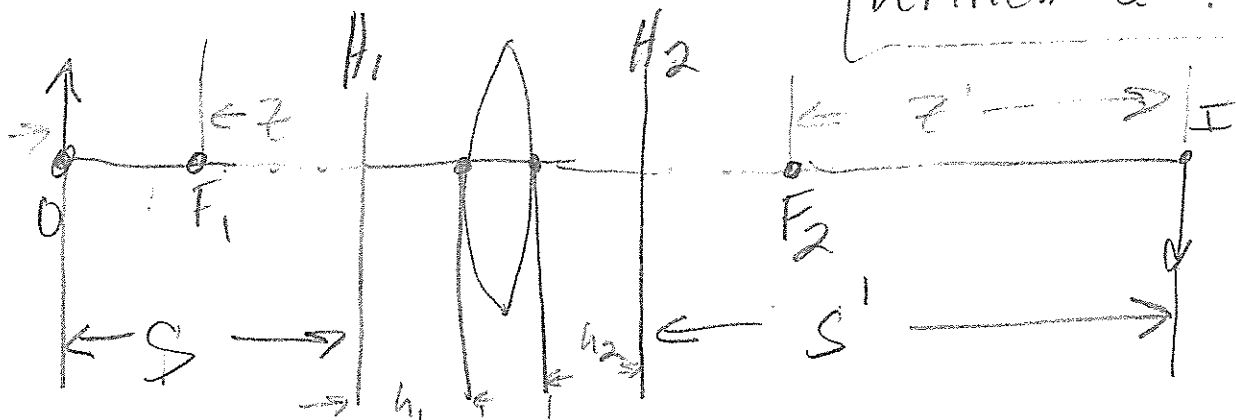
$$= \begin{pmatrix} m & 0 \\ -\phi & \frac{1}{m} \end{pmatrix} \quad E = \frac{1}{H} = \frac{1}{M_{az}}$$

$$m = \frac{x_1'}{x} = A + CS' = \frac{1}{D - CS}$$

UNIT Planes : = Principle Planes

xxxx

DEFINITION S.E. $M = +1$



These are the planes that are EQUIV. TO VERFAC >
i.e. PP $\Rightarrow$ V EQUIV. lens $\Rightarrow$ H1, H2

SET $m=1$ & solve

Principle Poles

(5)

$$h_1 = \frac{D-4}{C}$$

$$h_2 = \frac{1-A}{C}$$

Thru lens

$$O = \begin{pmatrix} 1 & s' \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ -\phi & 1 \end{pmatrix} \begin{pmatrix} 1 & -s \\ 0 & 1 \end{pmatrix}$$

$$= \begin{pmatrix} 1 - \phi s' & s' \\ -\phi & 1 \end{pmatrix} \begin{pmatrix} 1 & -s \\ 0 & 1 \end{pmatrix}$$

$$= \begin{pmatrix} 1 - \phi s' & s s' \phi - s + s' \\ -\phi & 1 + \phi s \end{pmatrix}$$

$$G=0$$

$$\frac{1}{s s'} \parallel s - s' + s s \phi = 0$$

$$\frac{1}{s'} - \frac{1}{s} = -\phi$$

$$\Rightarrow \frac{1}{s'} - \frac{1}{s} = -\phi$$

Plug in de power for shute lens
? we get lensmaker:

$$\frac{1}{s'} - \frac{1}{s} = (n_2 - 1) \left(\frac{1}{R_1} - \frac{1}{R_2} \right)$$

let $z = s - f_1$ $z' = s' - f_2$ (6)

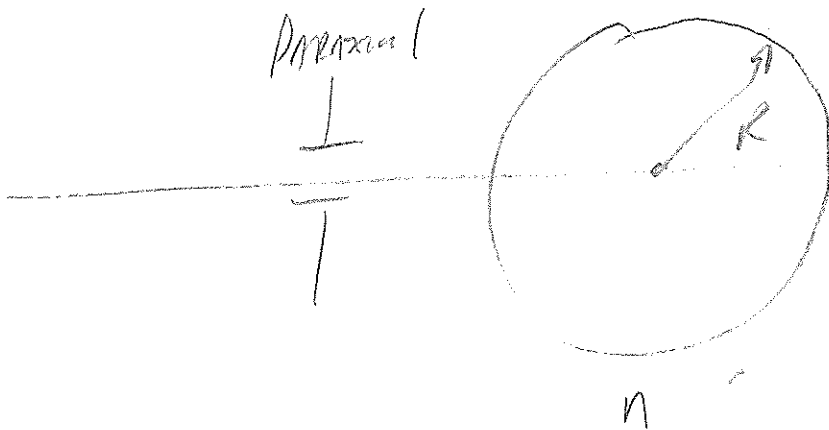
$$\Rightarrow \boxed{zz' = -f_1 f_2} \quad \text{Newton's Form}$$

Ex 2

Glass Ball as thick lens

$n = 1.5$ $R = 3 \text{ cm}$

$d = 2R$



$\phi_1 = \frac{n-1}{R} = \frac{1}{6}$
(3cm)ⁿ

$\phi_2 = \frac{1-n}{R} = -\frac{1}{6}$
(-3cm)ⁿ

$S = \begin{pmatrix} A & B \\ C & D \end{pmatrix}$

$= \begin{pmatrix} 1 - \frac{\phi_1 d}{n} & d \\ -(\phi_1 + \phi_2 - \frac{d\phi_1\phi_2}{n}) & (1 - \frac{\phi_2 d}{n}) \end{pmatrix}$

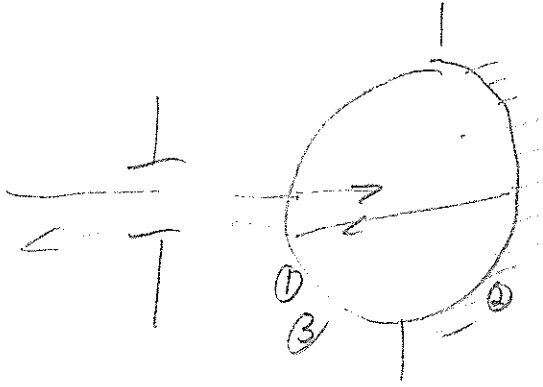
Where is Back focal point?

$S'_{BFL} = \frac{-A}{C} = \frac{1 - \frac{\phi_1 d}{n}}{\phi_1 + \phi_2 - \frac{d\phi_1\phi_2}{n}} = 1.5 \text{ cm}$

Ex 3

Reflecting glass ball.

7

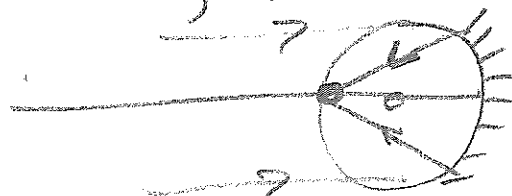


$$S = R_3 T_{23} R_2 T_{12} R_1$$

2/1/10

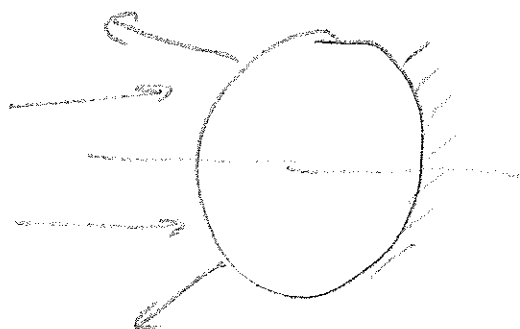
(3)

2) $n=4$; $A=D=0$, $s=s'=50$



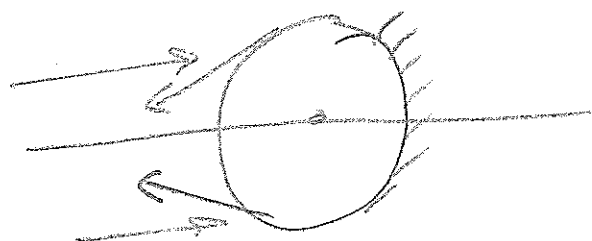
3) $1 < n < 2$

Plugging out



4) $2 < n < 4$

Converging lens



$l = -\infty$ to 0